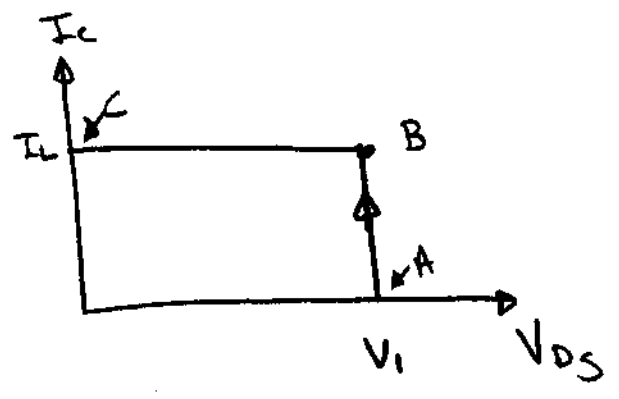
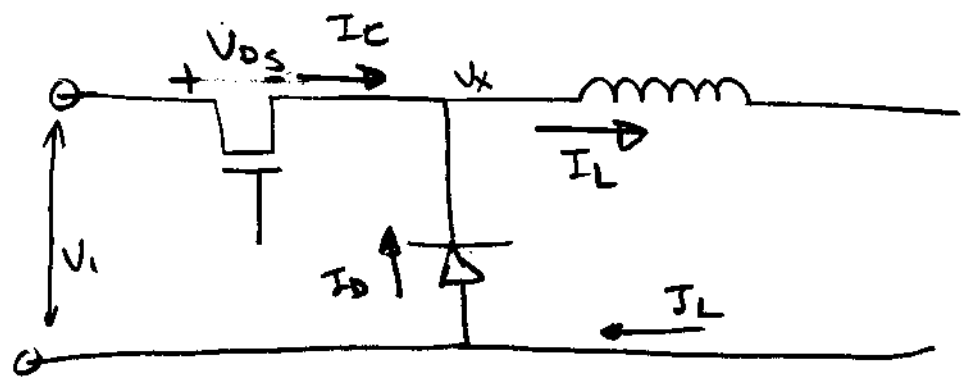


Turn-on problems with Buck transistors



- while MOSFET is off
 - I_L flows through the free-wheel diode
 - $V_{ds} = V_i$

- as MOSFET turns on $I_c \uparrow$, $I_d \downarrow$

$$I_L = I_d + I_c$$

- as $I_c \uparrow$

- I_c goes from 0 to I_L

- I_D goes from I_L to 0

\Rightarrow while I_c $0 \rightarrow I_L$, $I_D \neq 0$

- since $I_D = 0$, $V_D = V_g$ and $V_{DS} = V_i - V_g$

\Rightarrow as MOSFET turns ON

$$V_{DS} \approx V_i$$

$$I_c = I_L$$

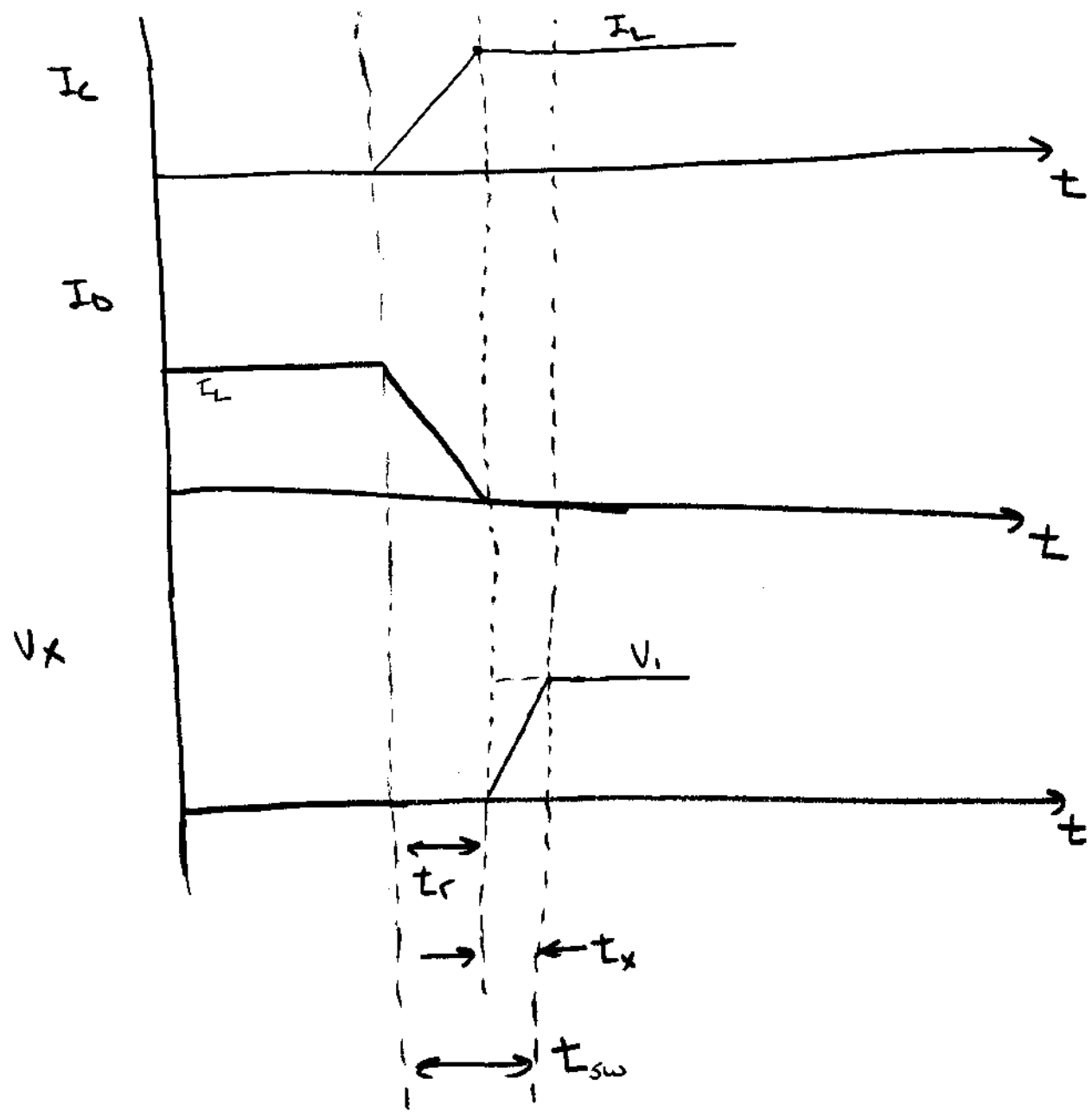
\Rightarrow on graph, Transition from
 (A) to (B).

\Rightarrow once $I_D = 0$, V_x is free to rise to V_i

$$I_c = I_L$$

$$V_{DS} = V_i \rightarrow 0$$

\Rightarrow on graph, Transition From B \rightarrow C.



During t_r , $V_{DS} = V_i$, $\langle I_c \rangle = \frac{I_L}{2}$

$$\langle P \rangle = V_{DS} \langle I_c \rangle = \frac{V_i I_L}{2}$$

$$\langle P \rangle \text{ per cycle} = \langle P \rangle \frac{t_r}{T_s} = \frac{V_i I_L}{2} \frac{t_r}{T_s}$$

During t_x , $I_L = I_L$, $\langle V_{DS} \rangle = \frac{V_1}{2}$

$$\langle P \rangle = \langle V_{DS} \rangle I_L = \frac{V_1 I_L}{2}$$

$$\langle P \rangle_{\text{per cycle}} = \langle P \rangle \frac{t_x}{T_s} = \frac{V_1 I_L}{2} \frac{t_x}{T_s}$$

So Total switching power dissipation

$$\langle P \rangle_{sw} = \frac{V_1 I_L}{2} \left(\frac{t_x + t_r}{T_s} \right) = \frac{V_1 I_L}{2} \frac{t_{sw}}{T_s}$$

TURN-ON Switching loss

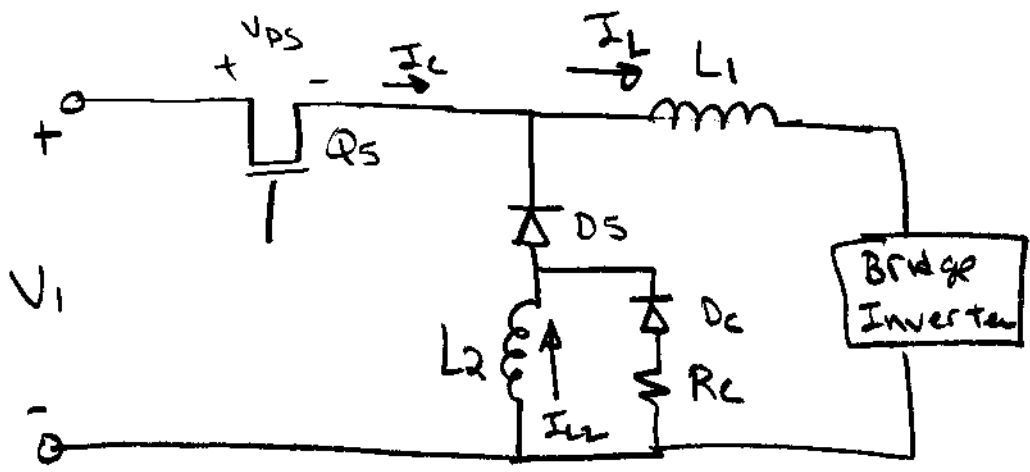
Note: Book states that $t_x \ll t_r$ so

$$\langle P \rangle_{sw} \approx \frac{V_1 I_L}{2} \frac{t_r}{T_s}$$

- For turn-off, we would trace out path C → B - A

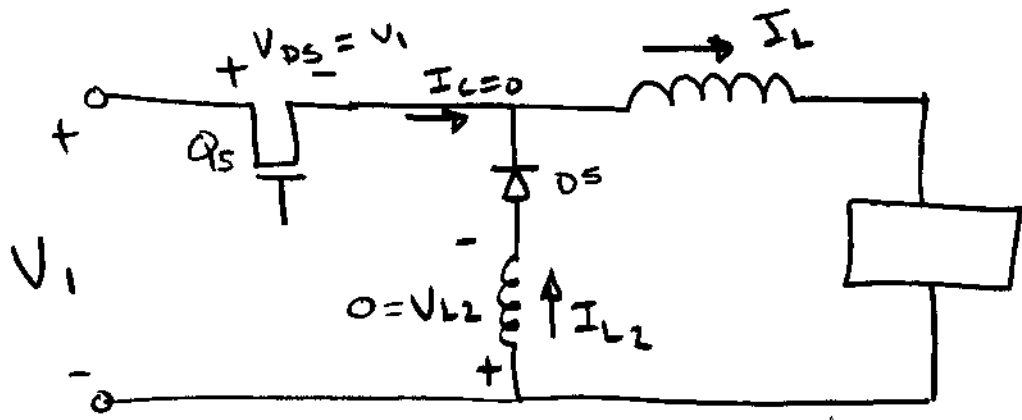
- Same equation for $\langle P \rangle_{sw}$ except that the switching times would be numerically different.

Buck Turn-on snubber



- Idea, while $I_c \rightarrow 0$ to I_L , keep $V_i = \text{small}$

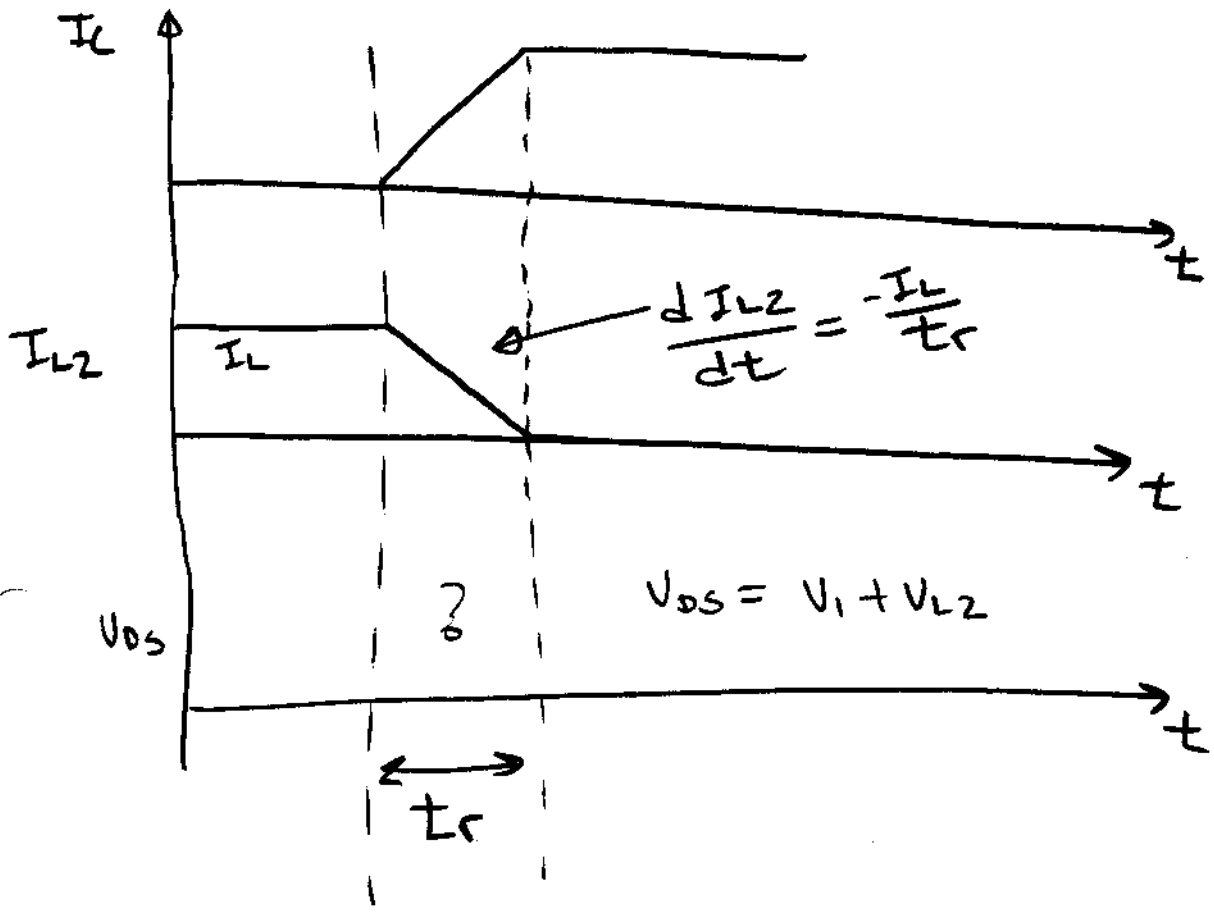
- while $Q_s = \text{OFF}$ we have



$$I_L = I_{L2}, \quad V_{L2} = 0 \Rightarrow \text{short}$$

$$I_c = 0$$

- Now look at when Q5 turns on



$$V_{L2} = L_2 \frac{dI_L}{dt} = -L_2 \frac{I_L}{t_r}$$

Choose L_2 so that $V_{DS} = 0$

$$0 = V_1 + V_{L2} = V_1 - L_2 \frac{I_L}{t_r}$$

$$\Rightarrow \boxed{L_2 = \frac{V_1 t_r}{I_L}}$$

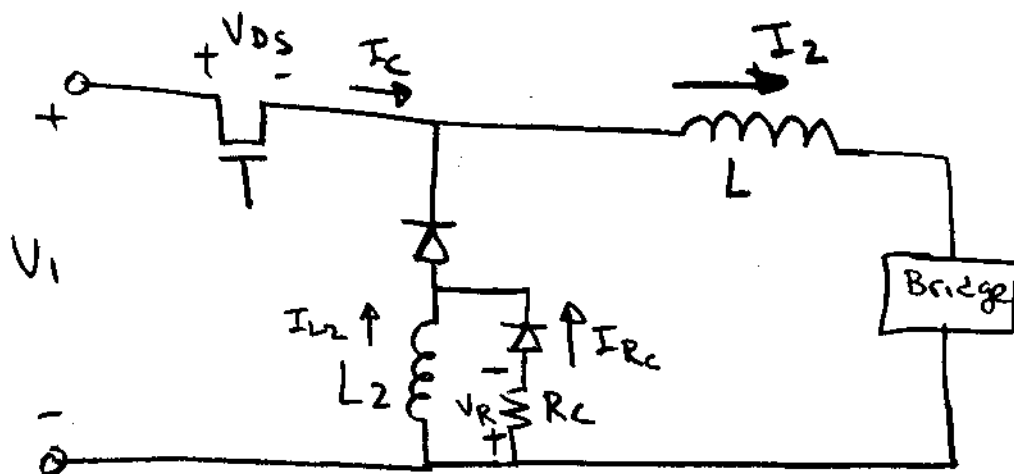
- The large $\frac{dI}{dt}$ causes a big V_{L2}

$$- V_{DS} = V_1 + V_{L2}$$

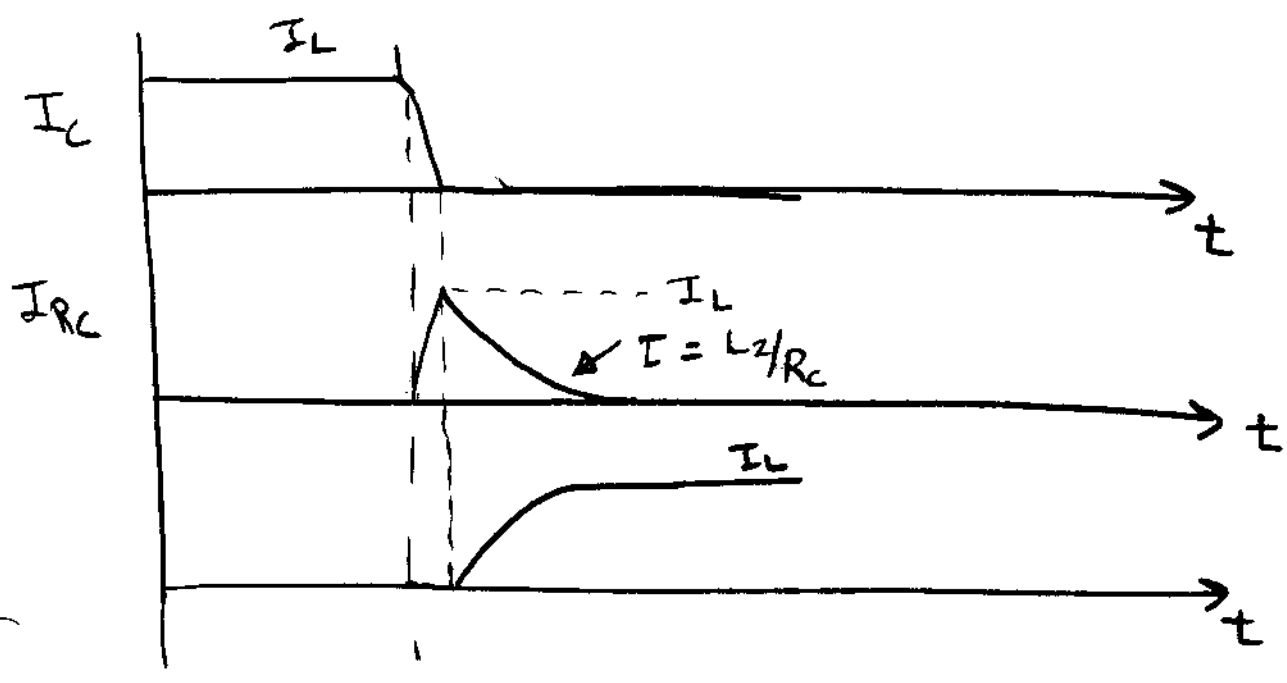
$$= V_1 + L_2 \frac{dI}{dt} = \text{big}$$

⇒ Kill MOSFET SWITCH

- add a parallel Resistor to snub Voltage SPIKE.

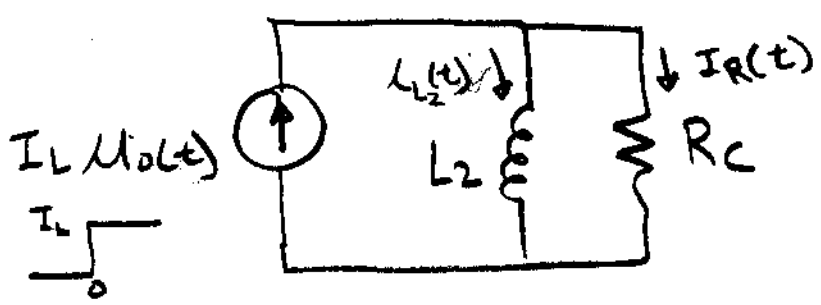


- At the instant of turn-off, there is NO current through L_2

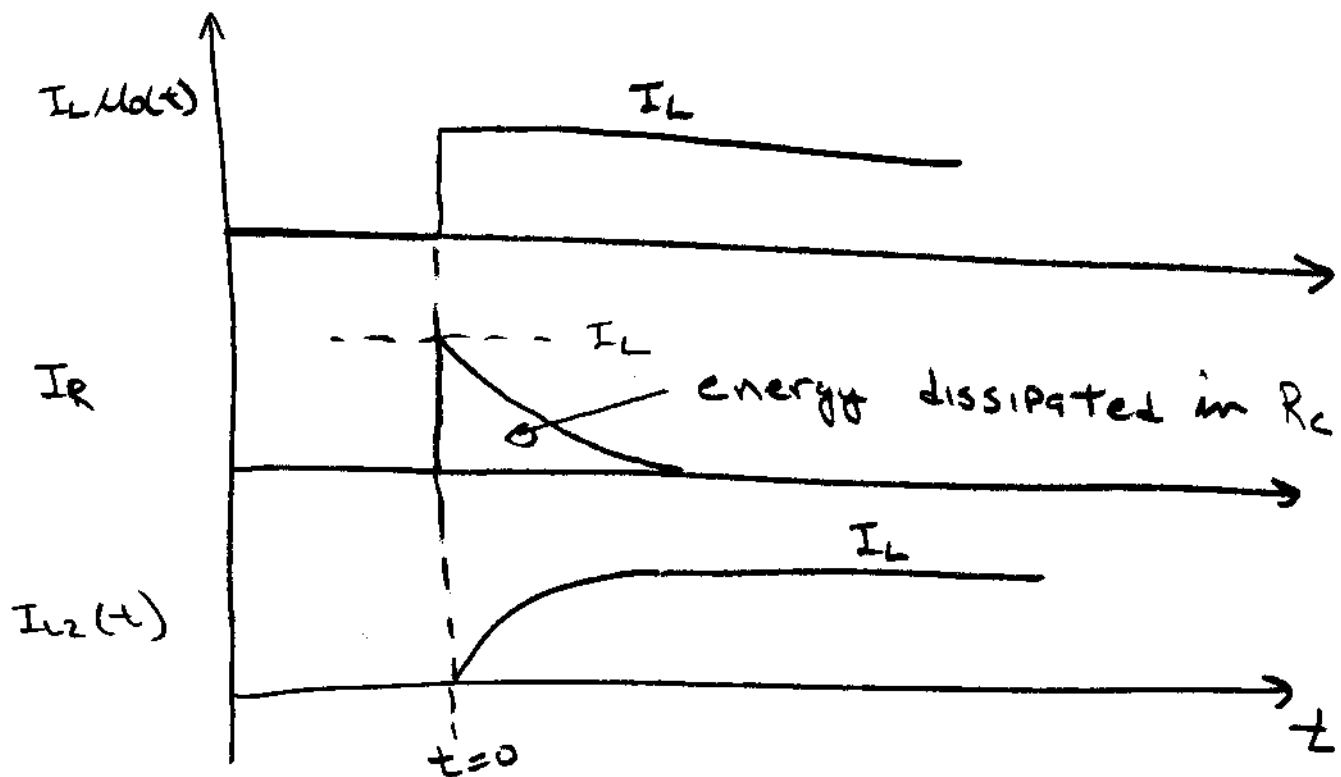


How much power is dissipated in R_c ?

Equivalent circuit



- How much Energy is dissipated in R_c



$$I_R(t) = I_L e^{-t/\tau} \quad ; \quad \tau = L/R_c$$

$$P_R = I_R^2 R_c$$

$$P_R(t) = I_L^2 R_c e^{-2t/\tau}$$

$$\begin{aligned} E_R &= \int_0^{\infty} P_R(t) dt = \int_0^{\infty} I_L^2 R_c e^{-2t/\tau} dt \\ &= \left[-I_L^2 R_c \frac{\tau}{2} e^{-2t/\tau} \right]_0^{\infty} = \frac{I_L^2 R_c \tau}{2} \end{aligned}$$

$$E_R = \frac{I_L^2 R_c}{2} \frac{L_2}{R_c} = \underbrace{\frac{1}{2} L_2 I_L^2}$$

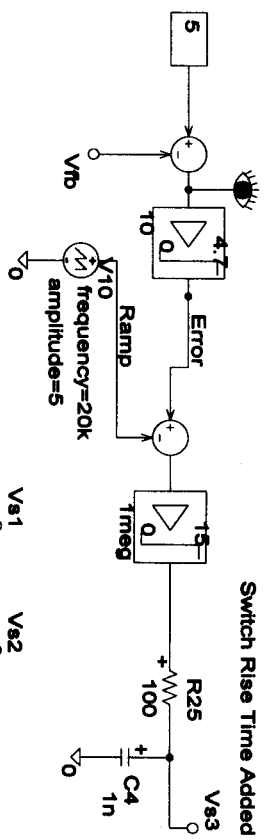
I_L = peak current through L_2

$$E_R = \frac{1}{2} L_2 I_L^2 = \text{Energy dissipated per cycle.}$$

$$P_R \Big|_{\text{Avg}} = E_R F_s$$

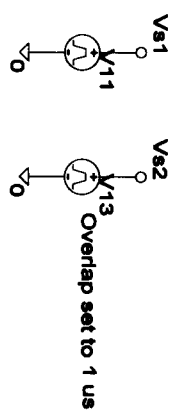
$$P_R \Big|_{\text{Avg}} = \frac{1}{2} L_2 I_L^2 F_s$$

436A



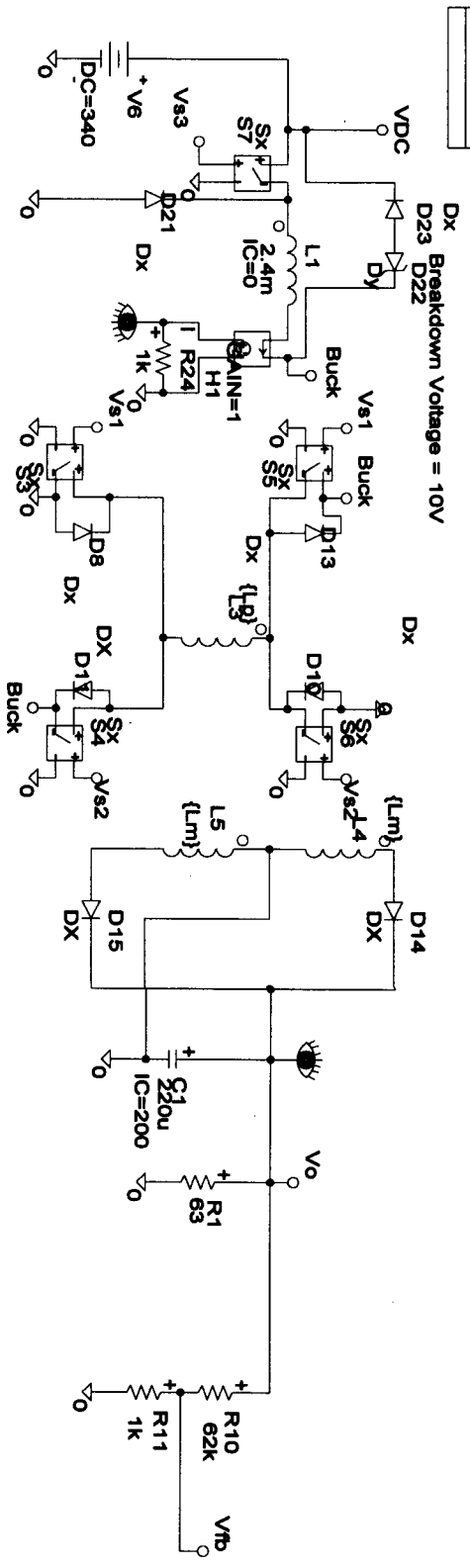
PARAMETERS:
Nm 2
Np 1
Lp 11.852m

PARAMETERS:
Lm {Lp*(Nm*Nm)/(Np*Np)}



Coupling=0.9998

K1
L5
L4
L3



Dx Breakdown Voltage = 10V

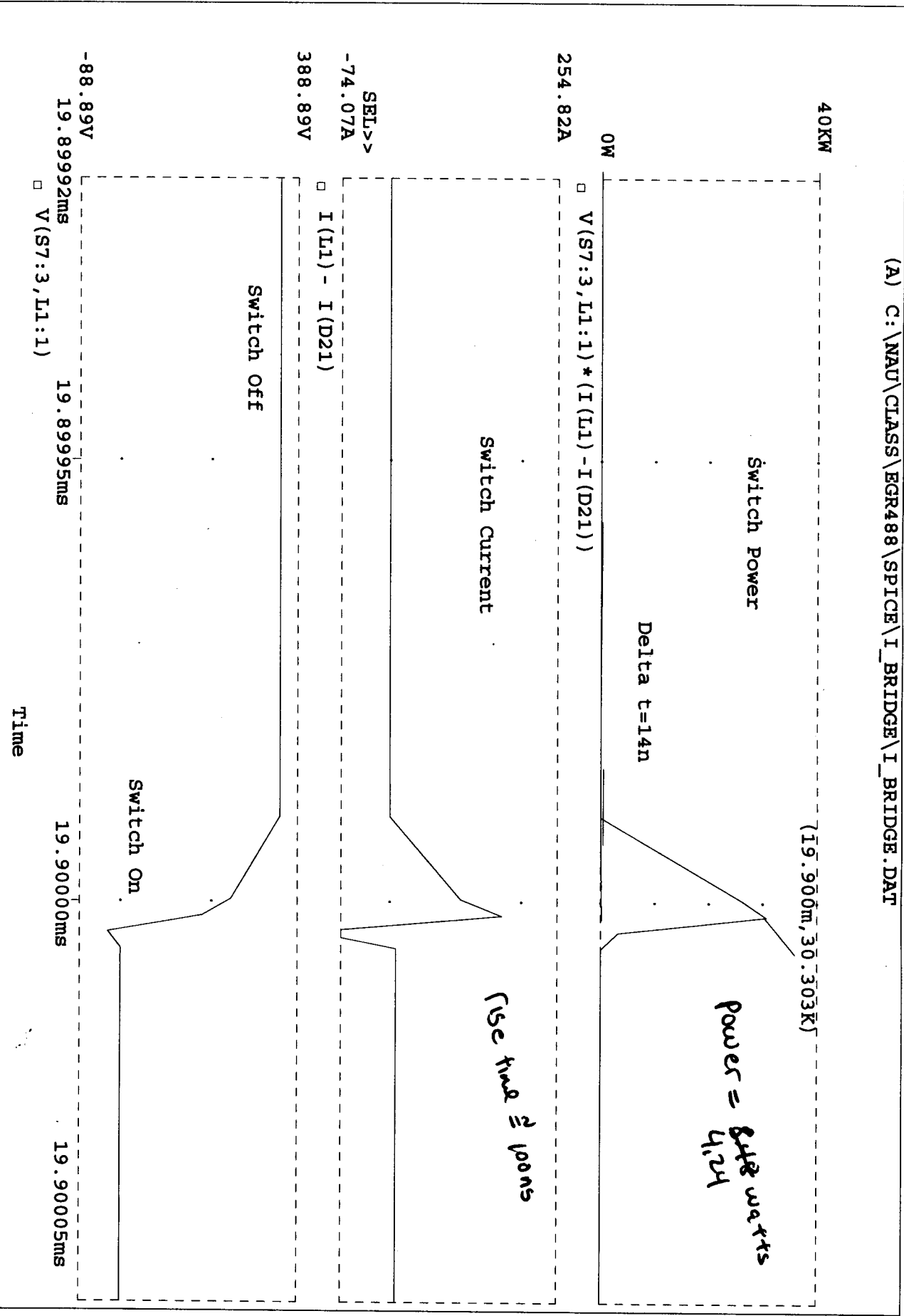
Northern Arizona University
College of Engineering and Technology
Flagstaff, AZ 86011-1560
(520) 523-1448

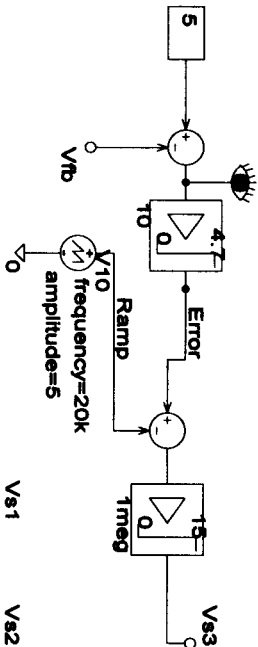
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Revision:

Homework=1
Problem=1
CLASS=EGR368
Semester=Fall 92
Prof.=Herliker
January 1, 2000

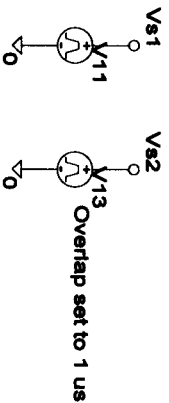
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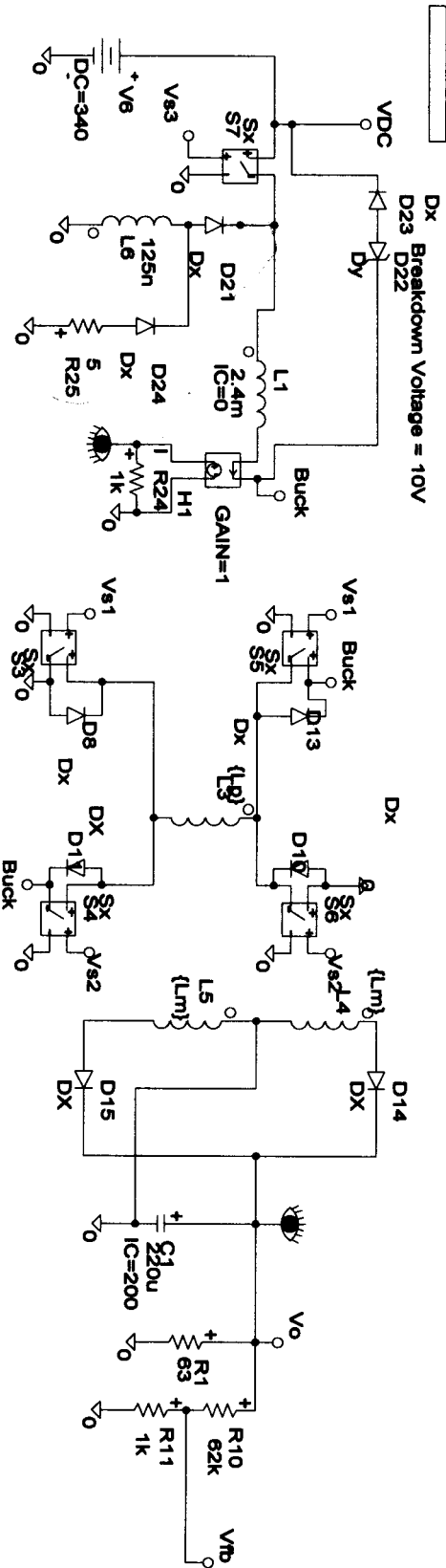
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PARAMETERS:
 Lm {Lp*(Nm*Nm)/(Np*Np)}



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L5
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L3



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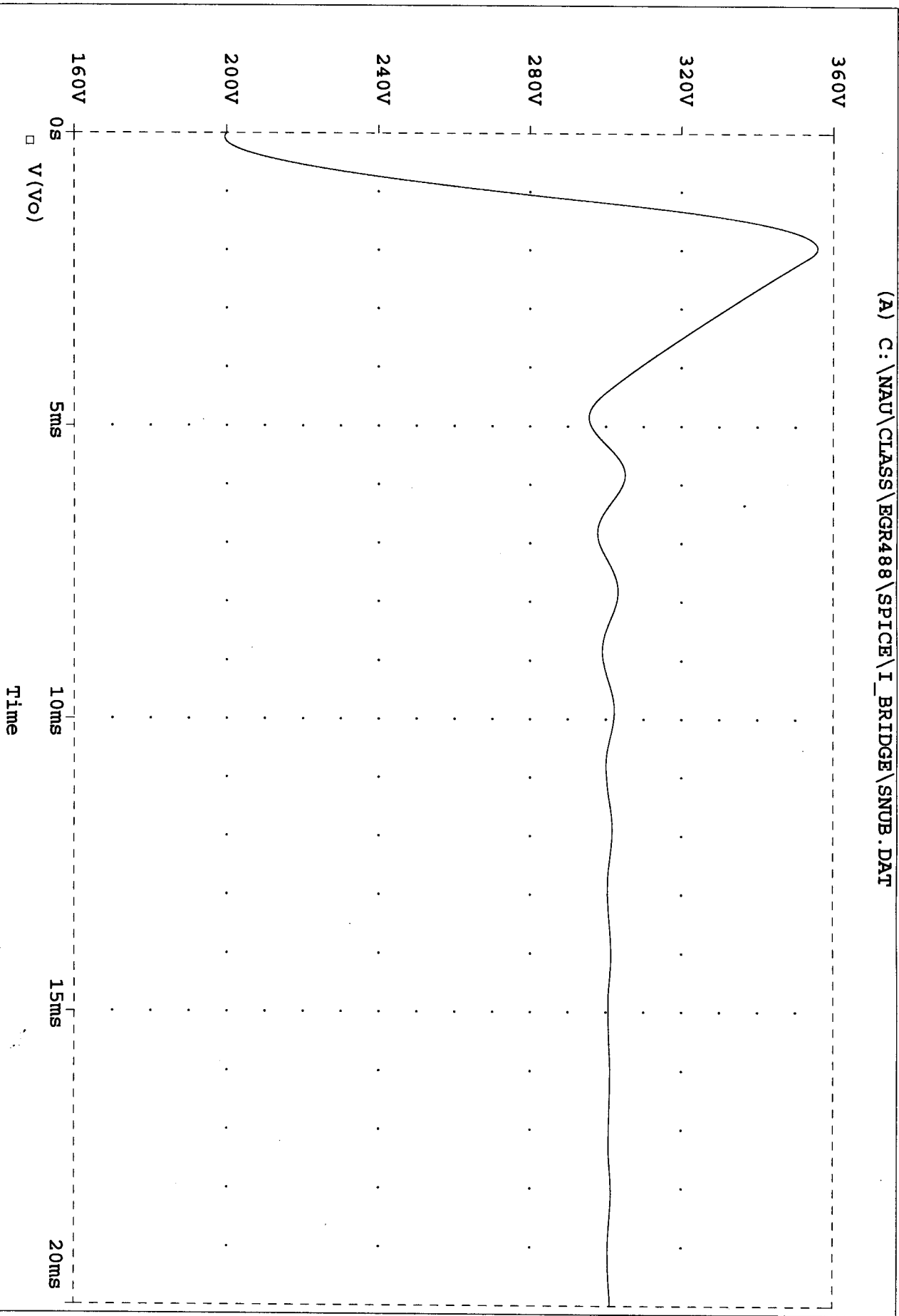
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 Problem=1
 CLASS=EGR368
 Semester=Fall 92
 Prof.=Heritier
 January 1, 2000

Revision:

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Temperature: 27.0

(A) C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.DAT



Date: October 26, 1995

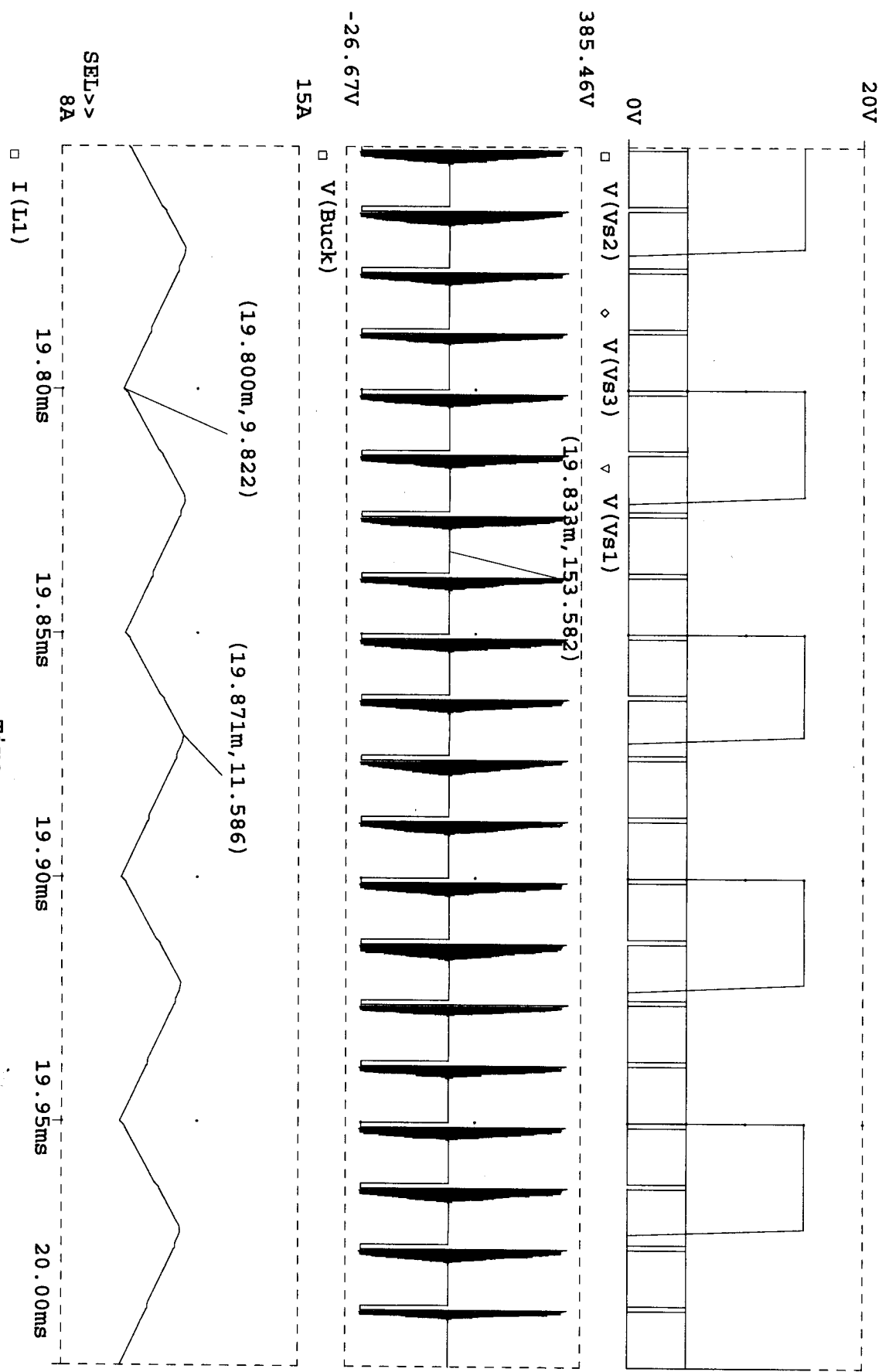
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Temperature: 27.0

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Date: October 26, 1995

Page 1

Time: 08:58:20

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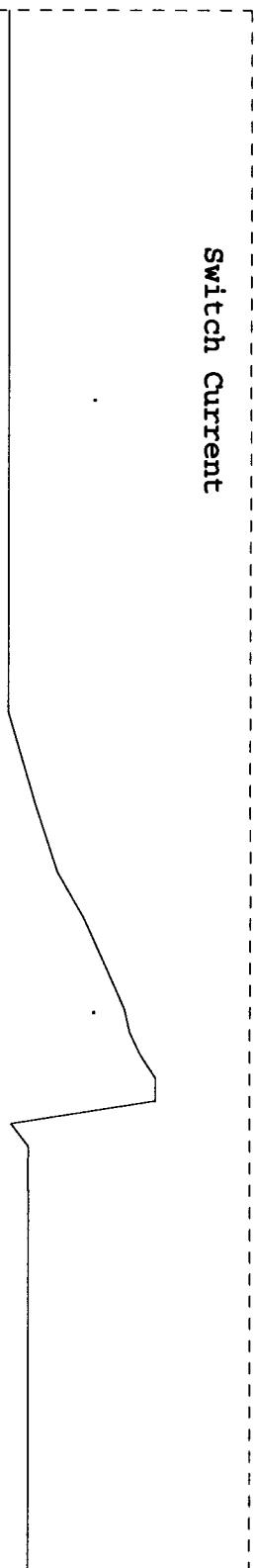
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Temperature: 27.0

(A) C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.DAT

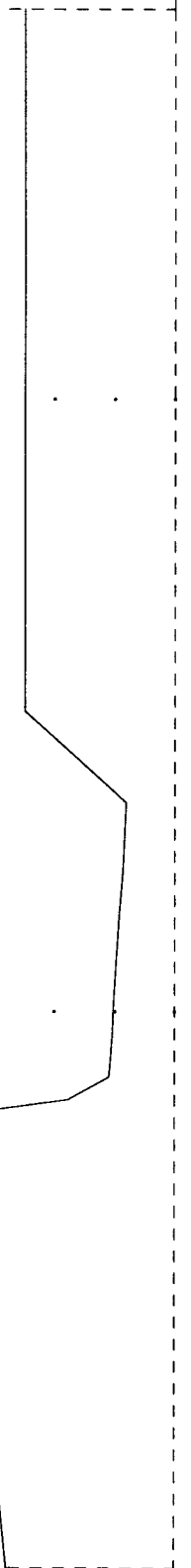
112.12A

Switch Current



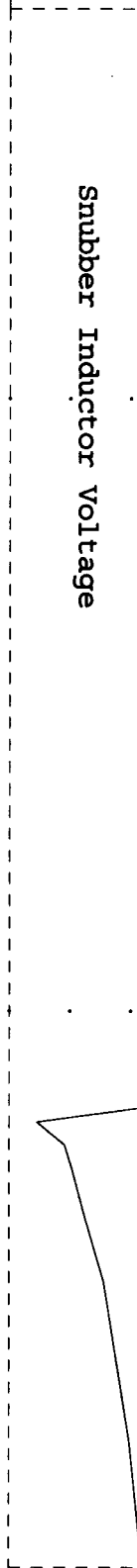
SEL>>
-27.27A

I (L1) - I (D21)



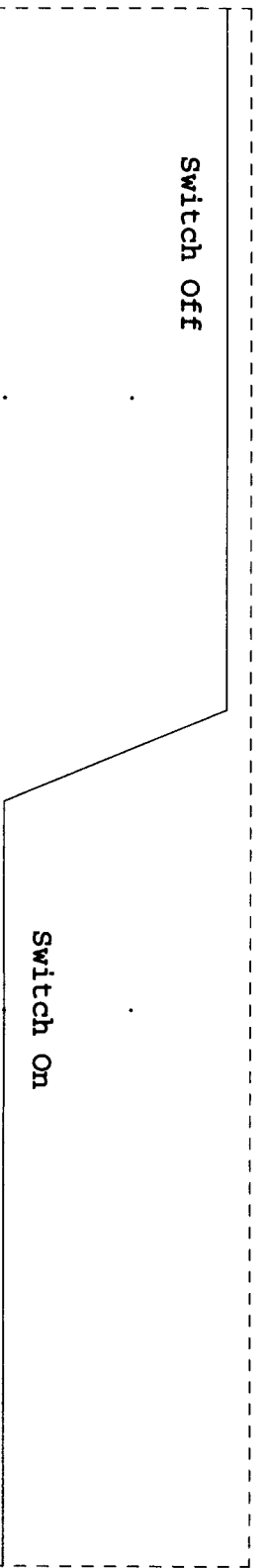
500V

Snubber Inductor Voltage



388.89V

V (D24:2)



Switch Off

Switch On

-88.89V

19.89992ms

19.89995ms

V (S7:3, L1:1)

19.90000ms

19.90005ms

Time

Date/Time run: 10/25/95 15:27:05 * C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.SCH

Temperature: 27.0

(A) C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.DAT

54.82W

(19.900m, 4.9813)

(19.900m, 46.987)

Switch Power

(19.900m, 445.780m)

200

P = 9.4mW

(I (L1) - I (D21)) * V(S7:3, L1:1)

-21.21W
254.82A

Switch Current

SEL>>
-74.07A

I (L1) - I (D21)

388.89V

Switch OFF

Switch On

-88.89V

19.89992ms

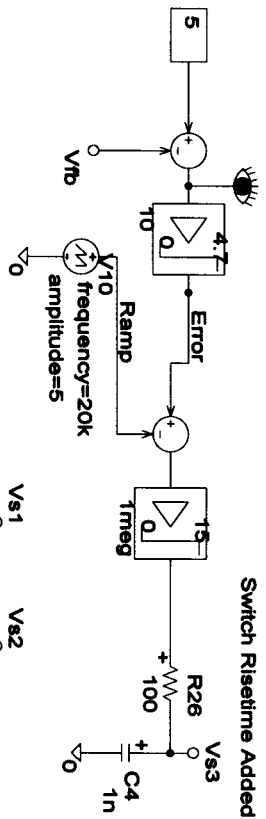
19.89995ms

19.90000ms

19.90005ms

V(S7:3, L1:1)

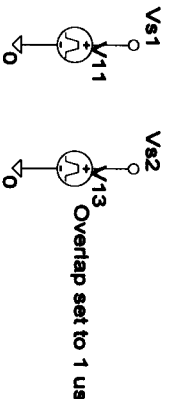
Time



Switch Risettime Added

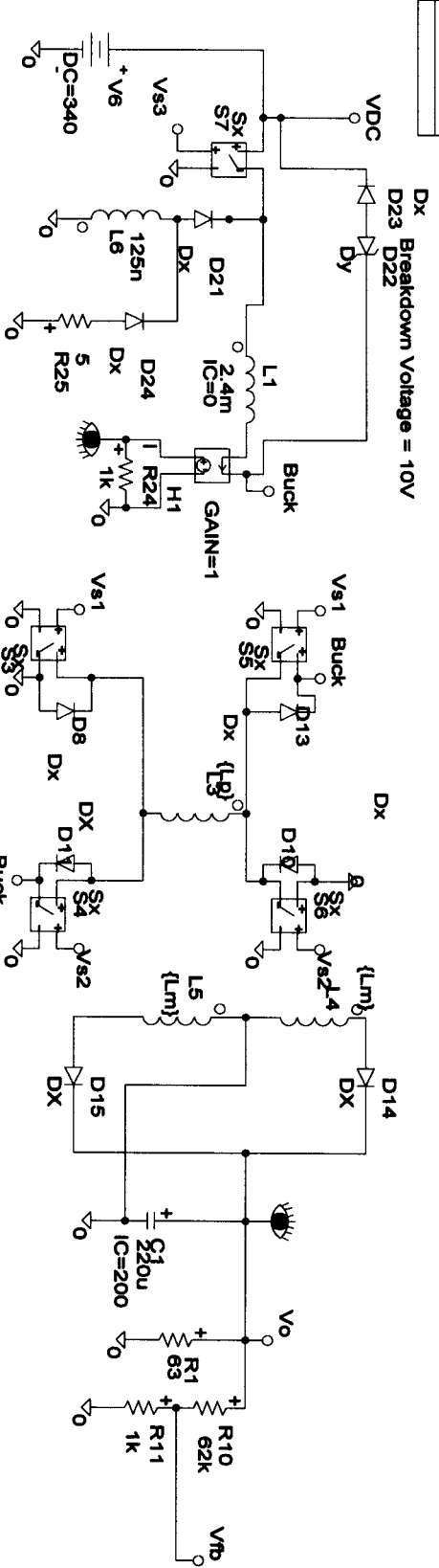
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Coupling=0.9998

K1
L5 L4 L3



Breakdown Voltage = 10V

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 College of Engineering and Technology
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 Problem=1
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 Semester=Fall 92
 Prof.=Hemitter
 January 1, 2000

H

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Date/Time run: 10/27/95 16:55:18

Temperature: 27.0

(A) C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.DAT

112.12A

Switch Current

-27.27A

400V

I (L1) - I (D21)

-400V

388.89V

V (D24:2)

Snubber Inductor Voltage

Switch Off

Switch On

SEL>>
-88.89V

V (S7:3,L1:1)

Time

19.89992ms

19.89995ms

19.90000ms

19.90005ms

(A) C:\NAU\CLASS\EGR488\SPICE\I_BRIDGE\SNUB.DAT

739.39W

Switch Power

Delta t=11n

(19.900m, 581.901)

Power = 63mW

SEL->
OW

121.27A

V(S7:3,L1:1)*(I(L1)-I(D21))

Switch Current

-30.22A

I(L1) - I(D21)

388.89V

Switch Off

Switch On

-88.89V

19.89992ms

19.89995ms

V(S7:3,L1:1)

19.90000ms

19.90005ms

Time